

Cryogenic Front-end for Astrophysics analog multiplexers and cryo-electronics

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Ecole de Microélectronique IN2P3 2015
17 - 22 mai 2015 - Fréjus

Observational astrophysics and cosmology from radio-astro to high-energy astro. :

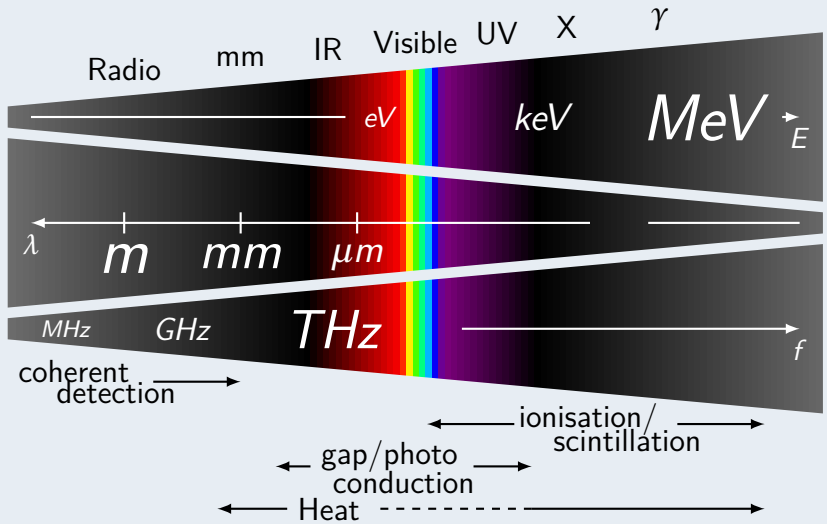
Astronomical sources

	f	λ	E	Astro. sources
Radio	< 300MHz	> 1m	< 1 μ eV	21cm redshifted
μ Wave	\approx 3GHz	\approx 10cm	\approx 10 μ eV	1 H (21cm line)
mm	\approx 300GHz	\approx 1mm	\approx 1meV	CMB
IR	\approx 300THz	\approx 1 μ m	\approx 1eV	interstellar dusts
Visible	\approx 500THz	\approx 600nm	\approx 2eV	stars, planet ...
UV	\approx 1PHz	\approx 300nm	\approx 4eV	Sun, stars
X	\approx 300PHz	\approx 1nm	\approx 1keV	X binaries
γ	> 30EHz	< 10pm	> 100keV	GRB

Arrays of sensors required to **fast and sensitive maps** of the sky.



Development of sensor technologies in many wavelength range.



"We must be **COOL**ed to be **sensitive**"
+
"**Array** are needed to do maps - do **images**
AND
integrate signal - **sensitivity** again"
=
Cryogenic Multiplexing



Outline

- 1 Analog multiplexers
 - Multiplexing as a modulation
 - Time domain multiplexing
 - Frequency domain multiplexing
- 2 Cryo-electronics
 - Cryogenic electronic devices
 - Semiconductor active devices
 - SQUID a superconducting active device
- 3 Applications
 - Millimeter domain to IR
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 - X domain



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Multiplexing general

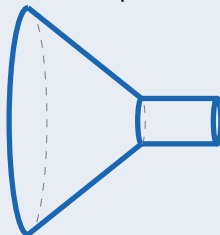
Transmission of N signals over 1 channel

INFORMATION

N data/signals



Multiplexer



TRANSMISSION

One channel



Introduced for telegraphy at the end of the 19th century and widely applied in **telecommunications** during the 20th century :

several telephone calls may be carried using one wire

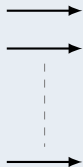


Multiplexing general

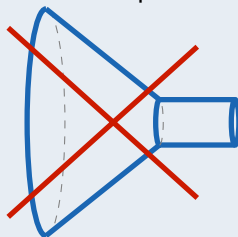
Transmission of N signals over 1 channel

INFORMATION

N data/signals



Multiplexer



TRANSMISSION

One channel

That is **not a real multiplexer**, because this need to reduces - **Data compression** - the transmitted informations to use the **same output channel capacity**



Multiplexing general

Transmission of **N** signals over **1** channel with **HIGHER** "capacity"

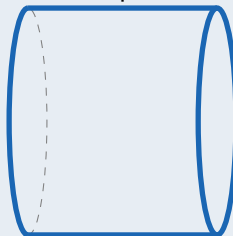
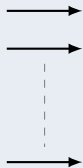
INFORMATION

TRANSMISSION

N data/signals

Multiplexer

One channel



To transmit N signals via One channel, the "channel" must provides better performances than for a single signal transmission.



Multiplexing notice



To transmit N signals *via* one channel, **the "channel" must provides better performances** than for a single signal transmission.

- ⇒ The increasing of the required performances are directly linked to the number N of multiplexed signals.
- ⇒ The affected performances are both :
 - Band Width
 - Dynamic / Signal to Noise Ratio

the multiplexing **divides the capacity of the high-level communication channel** into several **low-level sub-channels**, one for each message, signal or data to be transmitted.



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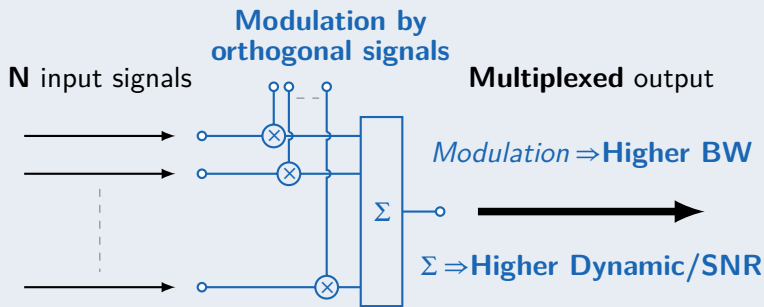
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Multiplexing as a modulation

There are intersections between modulation and multiplexing

Multiplexing = modulation of input signals by orthogonal signals :

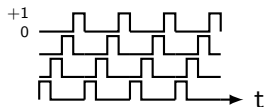


Orthogonal : **boxcar functions** or **carriers at different frequencies**.
Orthogonality \Rightarrow demultiplexer **able to recover each input signals without interference from the other**.



Orthogonal functions

- boxcar functions \equiv **sampling**

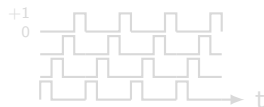


- carriers \equiv **modulation**
- linear codes \equiv **coding**

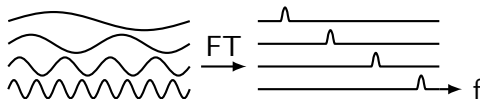


Orthogonal functions

- boxcar functions \equiv **sampling**



- carriers \equiv **modulation**

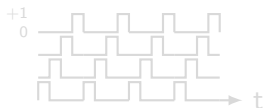


- linear codes \equiv **coding**



Orthogonal functions

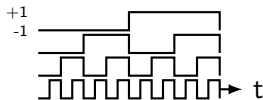
- boxcar functions \equiv **sampling**



- carriers \equiv **modulation**



- linear codes* \equiv **coding**



*. as used for error-detection/correction code. Especially, Hadamard/Walsh code could be used for multiplexing.

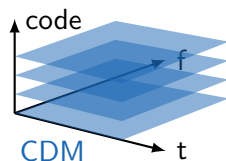
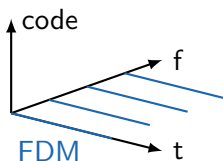
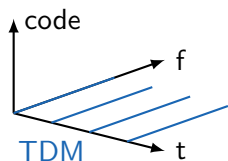


Multiplexing type vs standard modulations

- Multiplexing
 - **Time Domain Multiplexing (TDM)**
 - **Frequency Domain Multiplexing (FDM)**
 - Wave length Domain Multiplexing for optical fiber
 - Coded Domain Multiplexing (CDM)
- Coding
 - Amplitude Shift Keying (ASK)
 - Frequency Shift Keying (FSK)
 - Coded Division Multiple Access (CDMA)



Code as a third dimension ?



Multiplexing \Rightarrow spread spectrum

- Code is represented as a third dimension even if this is **not necessarily a physical dimension**.
- CDM is usually used to **spread the spectrum** of the multiplexed signal. But the code dimension is often a repartition both in time, in frequency and some times in amplitude.

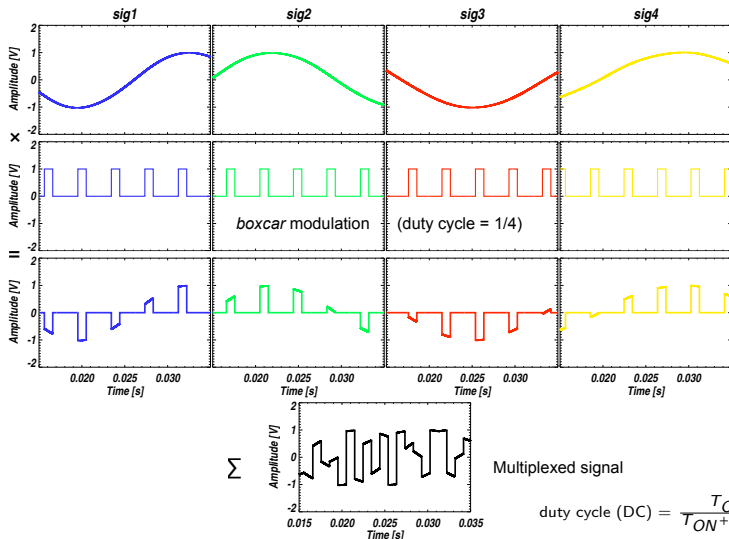


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Boxcar modulation + Summing

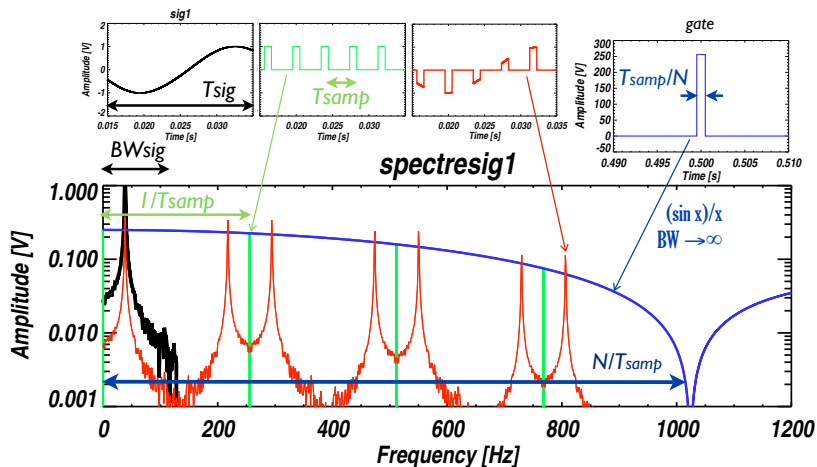


$$\text{duty cycle (DC)} = \frac{T_{ON}}{T_{ON} + T_{OFF}}$$

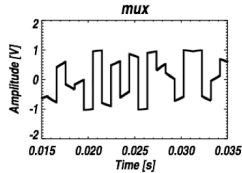
$\Rightarrow N \setminus \rightarrow DC \setminus \rightarrow BW \setminus$



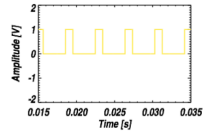
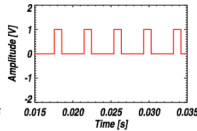
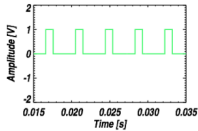
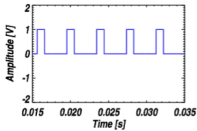
Spectrum of a boxcar modulation



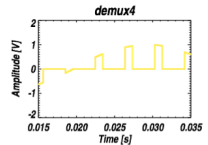
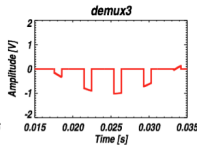
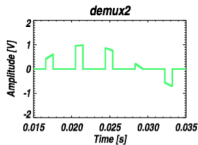
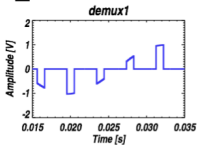
Demultiplexing - Demodulation



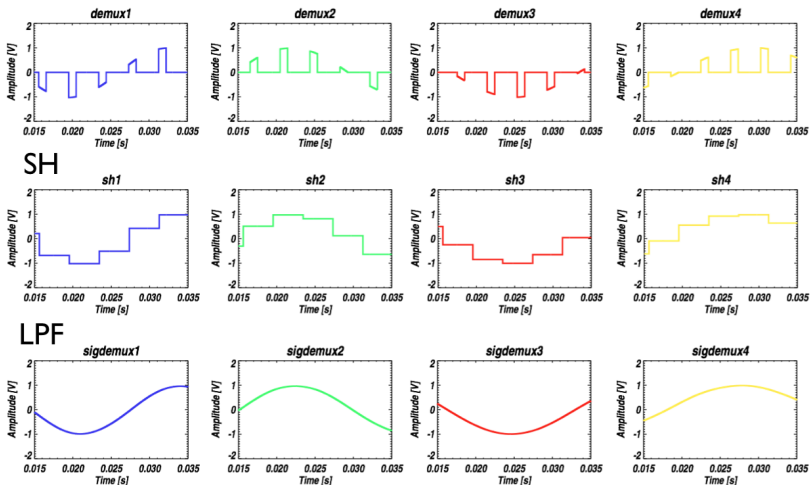
X



=



Demultiplexing - Sample and Hold



Sample and Hold (SH) + Low Pass Filtering (LPF)

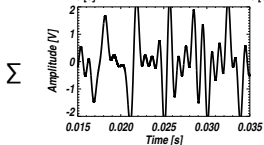
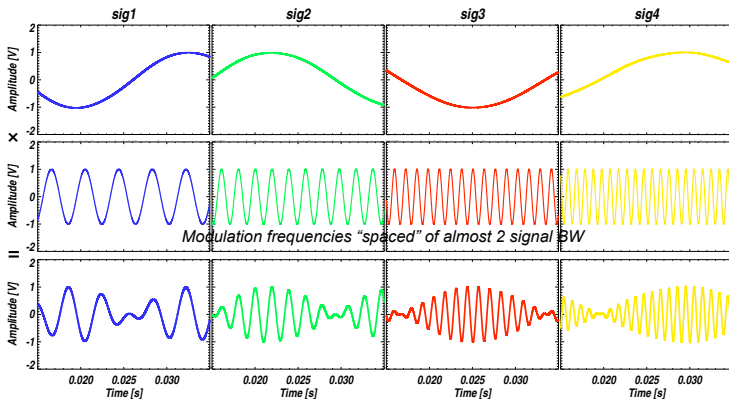


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Carrier modulation + Summing



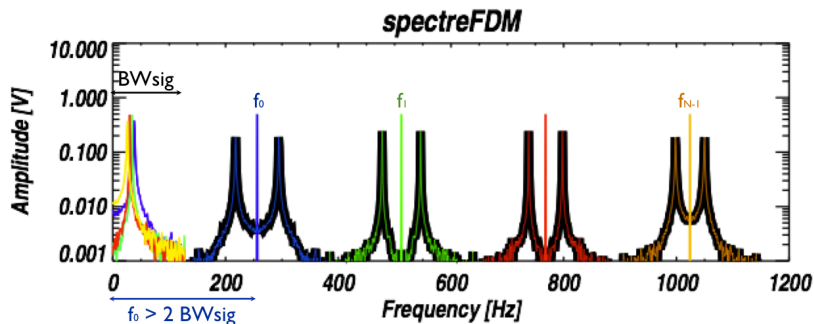
Multiplexed signal
(dynamique increased)

$$f_n - f_{n+1} > 2 \times \text{Signal BW}$$

$$\Rightarrow N \nearrow \rightarrow \text{MUX}_{\text{BW}} \nearrow$$



Spectrum of the frequency domain multiplexing

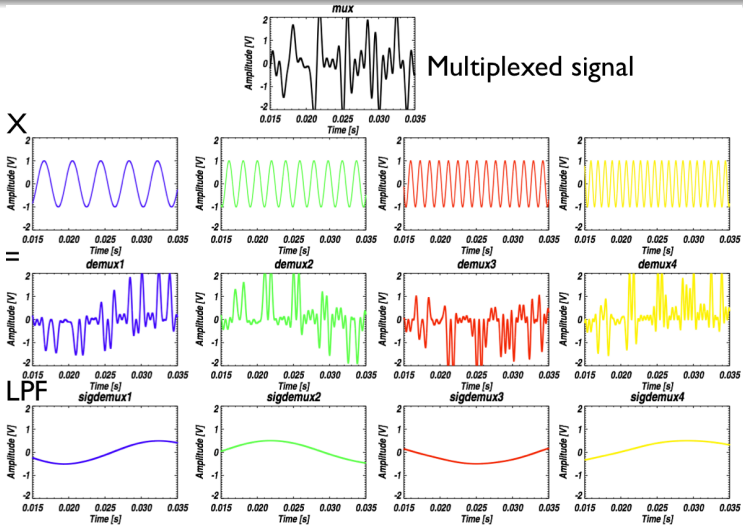


Increasing of the required band width

$$BW_{FDM} > 2 \times N \times BW_{sig}$$



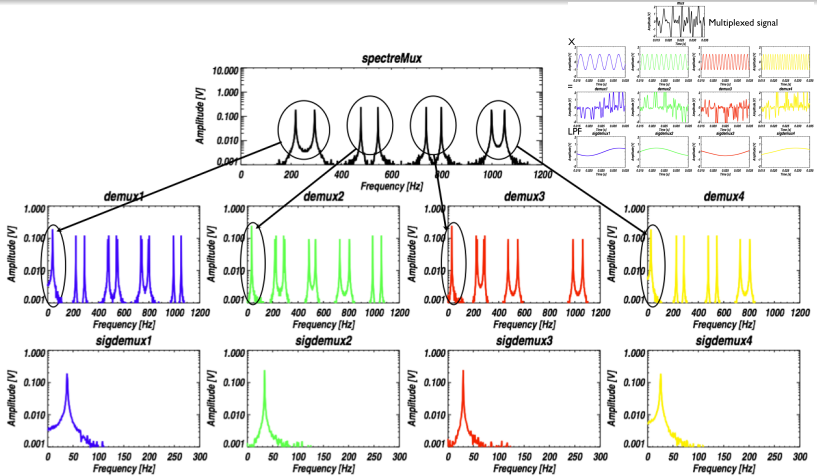
Demultiplexing \equiv Demodulation + filtering



Low Pass Filtering (LPF)



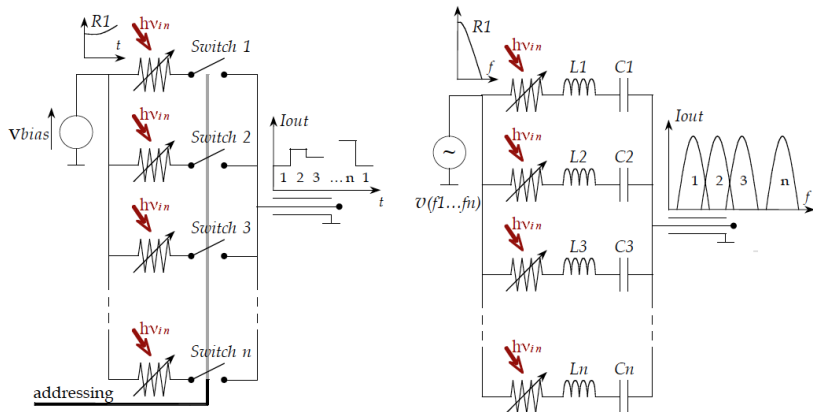
Demultiplexage \equiv Demodulation + filtering



Demodulation of each carrier i e each input signal
+ low pass filtering (LPF)



Topologie of a multiplexer



- **N switches or N LC filters**
- **N signals** for the addressing of the switch or the modulation



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Cryogenic electronic devices

- **Linear** amplifier or switches
 - **Passive** devices as **transformers** or resonant circuits
 - **Active** devices → *provide power amplification*
 - **Superconductor** devices as SQUIDs
 - **Semiconductor** devices as transistors

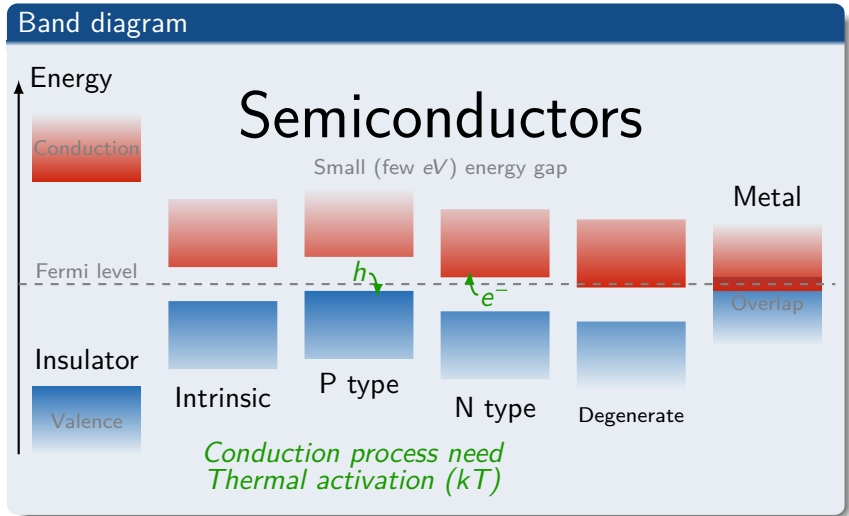
Semiconductor devices for amplification

- 1 **Field-effect** Transistors - FET
 - standard MOS & JFET
 - Hetero-junction FET *ie* HEMT
- 2 **Bipolar** transistors
 - Bipolar Junction Transistor - BJT
 - Hetero-junction Bipolar Transistor - HBT

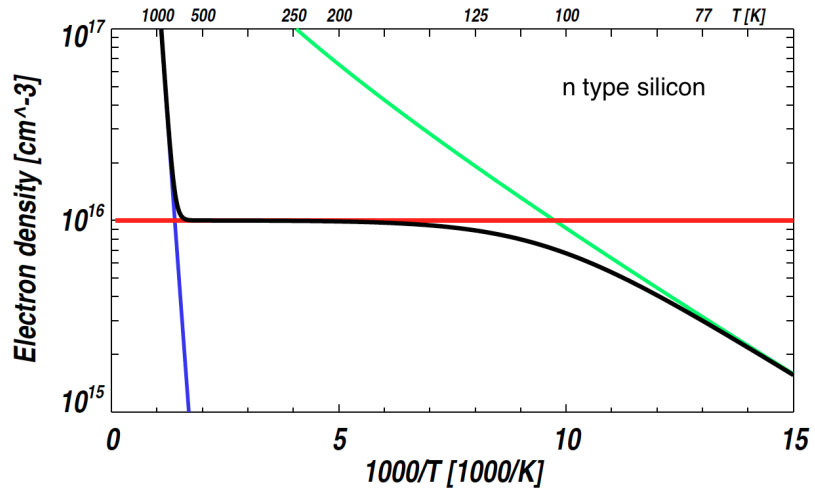
- **Non-linear** amplifier **parametric amplifier** or **mixer**



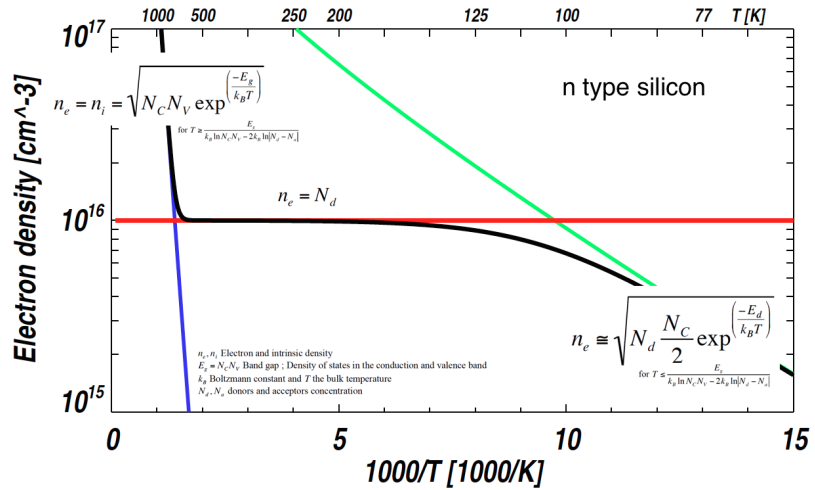
Solid-state physics and semiconductors



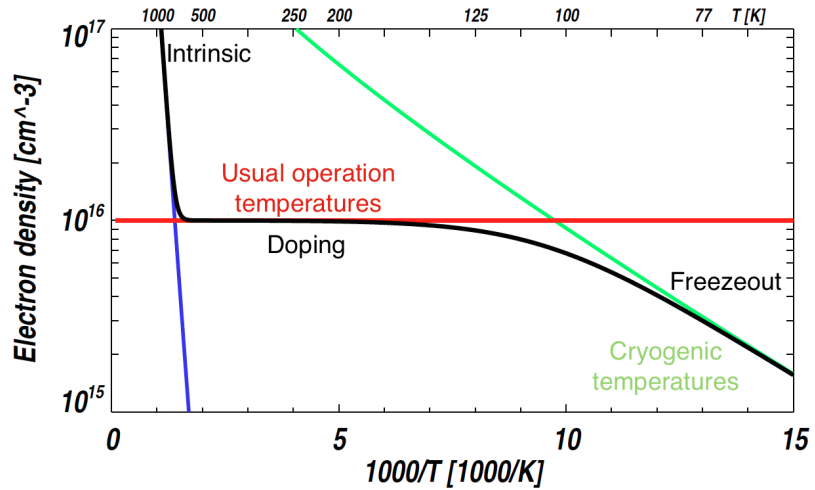
Solid-state physics and semiconductors (carriers density as function of T)



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Field-effect transistor technologies



Field Effect Transistor - FET

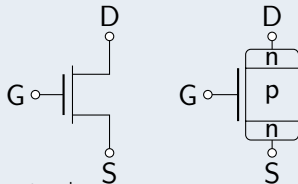
Field effect transistor uses **ELECTRIC FIELD** to **control** the output current

Different ways to **isolate** the grid

- 1 **INSULATOR** (as SiO₂)
→ MOSFET (Metal Oxide Semiconductor FET)
- 2 **Depleted region** of a reverse biased **pn JUNCTION**
→ JFET (Junction FET)
- 3 **Depleted wide band-gap** of an **HETEROSTRUCTURE** (as GaAs/AlGaAs)
→ HEMT (High Electron Mobility Transistor)

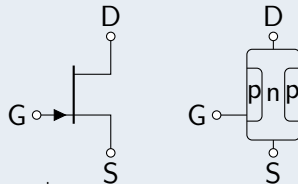


nMOS nodes & topology



enhancement-mode (depleted-mode MOS exists)

nJFET nodes & topology



depletion-mode

Parameters :

- **transconductance** $g_m = \frac{\partial I_D}{\partial V_{GS}}$
- capacitive input impedance \rightarrow close to ∞ at low freq.
- current gain not defined $\rightarrow Z_{IN}$ too large
- output impedance depends on the circuit (what the output is)



MOS and JFET transconductance

2 different operation modes for amplification

- 1 weak-inversion** for low consumption ; $I_D = I_{D0} \exp \frac{V_{GS} - V_{th}}{\eta V_T} \Rightarrow g_m = \frac{I_D}{\eta V_T}$
 $I_{D0} = I_D$ and $V_{GS} = V_{th}$, $\eta = 1 + \frac{C_D}{C_{ox}}$ at $V_T = \frac{k_B T}{q}$
- 2 the active mode** for low-noise analog amplifier

Linear low noise amplification \rightarrow *pinch-off* and **active mode** (saturation)

- $I_D(V_{DS}) \approx \kappa (V_{GS} - V_{th})^2$ with $\kappa = \begin{cases} \frac{\mu C_{ox}}{2} \frac{W}{L} & \text{for MOS} \\ \frac{I_{DSS}}{V_{th}} & \text{for JFET} \end{cases}$

- $|g_m| = \left| \frac{\partial I_D}{\partial V_{GS}} \right| \approx 2\kappa (V_{GS} - V_{th}) \propto \sqrt{I_D}$

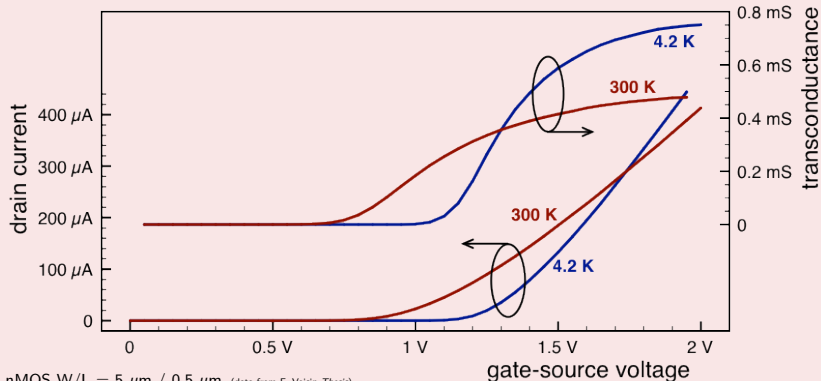
- $\mu(T) \propto T^{-\alpha} \rightarrow \mu \nearrow$ **at low temperature** $\Rightarrow g_m \propto \frac{\sqrt{I_D}}{T^\alpha}$



Cryogenic measurement of MOS transconductance

$$I_D(V_{DS}) \approx \frac{\mu C_{ox}}{2} \frac{W}{L} (V_{GS} - V_{th})^2$$

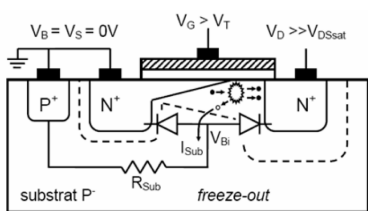
$$\Rightarrow |g_m| \approx \mu C_{ox} \frac{W}{L} (V_{GS} - V_{th}) \propto \frac{\sqrt{I_D}}{T^\alpha}$$



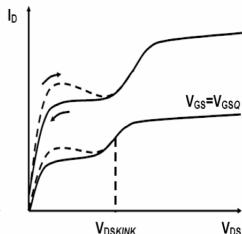
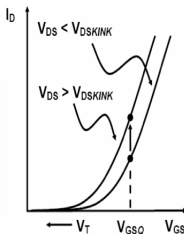
nMOS $W/L = 5 \mu\text{m} / 0.5 \mu\text{m}$ (data from F. Voisin Thesis)



MOS output characteristic and *kink effect*



• electron ◦ hole ◉ electron collision with the ionic lattice



F. Voisin - "uElec. Cryo. pour instru. bas bruit", Porquerolles 2007

At high V_D , e^- -hole pairs created by impact ionization mechanism.

- $e^- \rightarrow$ drain
- holes stay in the freeze-out bulk (increasing the bulk potential)
 \Rightarrow add a "potential control" in addition to V_{GS}

Kink effect is stronger in nMOS as compared to pMOS

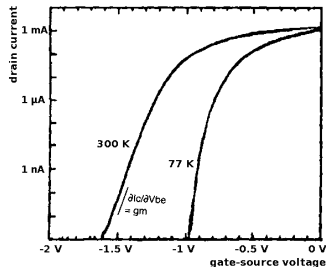
Solution : adding many bulk contact around the MOS



Cryogenic measurement of JFET transconductance

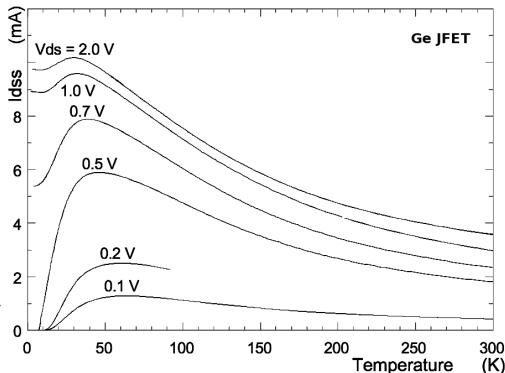
$$I_D(V_{DS}) \approx I_{DSS} \left(1 - \frac{V_{GS}}{V_{th}}\right)^2$$

$$\Rightarrow |g_m| \approx 2I_{DSS} \left(1 - \frac{V_{GS}}{V_{th}}\right) \propto \sqrt{I_D} I_{DSS}$$



Goldberg et al - Characterization of cryo Si JFET

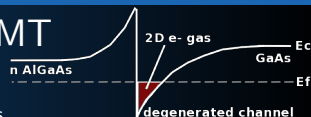
Ward et al - Dev. of Cryo Ge JFET ->



Si JFET for 77 K applications and Ge JFET for 4 K (but there are very few Ge commercial technology)

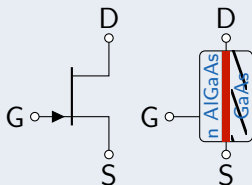


High Electron Mobility Transistor - HEMT



Charge carriers are "induced" to 2D layer rather than created by dopants

AsGa HEMT nodes & topology



2D electron gas (typ. 100Å)

HEMT technologies (JFET with heterojunction)

- **Very high e^- mobility** → **high g_m**
- High operation frequency up to mm wavelengths
- e^- conduction spatially separated from donor impurities → **no ionized scattering** (collisions with impurities)

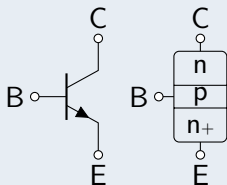
- Allows operation down to **sub-Kelvin temperatures** (degenerated)
- Suffer from **1/f noise** (crystal defects in interface and residual doping → traps and G-R noise)



Bipolar transistor technologies



Nodes & topology



Bipolar transistor technologies

Thin semiconductor material common to 2 junctions :

- **Homojunctions** Si/Si
→ Bipolar Junction Transistor - **BJT**
- **Heterostructure** III/V as InP/InGaAs or IV/IV as Si/SiGe
→ Heterojunction Bipolar Trans. - **HBT**

Parameters :

- **transconductance**
- **current gain**
- **input impedance**

$$g_m = \frac{\partial I_C}{\partial V_{BE}}$$

$$\beta = \frac{\partial I_C}{\partial I_B}$$

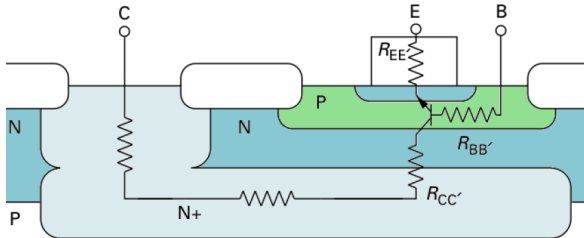
$$h_{11} = \frac{\partial V_{BE}}{\partial I_B} = \frac{\beta}{g_m}$$

- output impedance depends on the circuit (not an issue)



Bipolar access resistances R'

At cryogenic temperatures, weakly doped semiconductor suffer from freeze-out \Rightarrow **increasing of the access resistances**



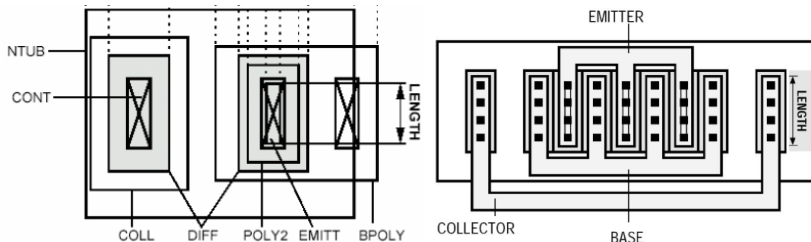
$R_{BB'}$ and $R_{EE'}$ access resistances are combine in a unique R'

$$R' = \frac{R_{BB'}}{\beta} + \frac{(\beta + 1)R_{EE'}}{\beta}$$



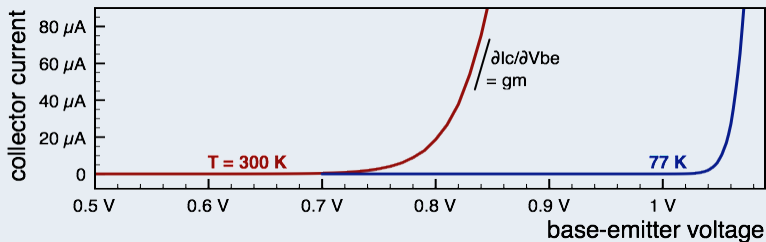
Multiple access to reduce parasitic resistances

Single vs multiple (NPN243) B, E and C acces :



Transconductance - g_m

Drift diffusion theory $I_C = I_{C0} \exp \frac{V_{BE}}{V_T}$ with $V_T = \frac{k_B T}{q}$



recombinations, carrier mean free path, thermal decoupling and R'

$$g_m = \frac{\partial I_C}{\partial V_{BE}} = \frac{I_C}{V_T} = \frac{q I_C}{k_B T} \quad \Rightarrow \quad g_m \Big|_{T_{\text{cryo}}} = \frac{\frac{q I_C}{\eta k_B T_e}}{1 + R' \frac{q I_C}{\eta k_B T_e}}$$



Current gain β and input impedance

Degraded BJT current gain at low temperatures

$$\beta \propto \exp \frac{\Delta E_g}{k_B T} \quad \text{with} \quad \Delta E_g = E_{gE} - E_{gB} < 0$$

ΔE_g : difference in band gap between the emitter and the base regions and induced by **doping - band gap narrowing**

Example of common commercial transistor : 2N2222 BJT

measured β go from **225** to **35** from room temperature to 77 K

$$h_{11} = \frac{\beta}{g_m} :$$

$$\text{Considering } I_C = 1\text{mA} \rightarrow h_{11(T=300\text{K})} = \frac{225}{39 \text{ mS}} \approx 6 \text{ k}\Omega$$

$$h_{11(T=77\text{K})} = \frac{35}{150 \text{ mS}} < 250\Omega \Rightarrow \text{fails } Z_{in} > Z_S \text{ at lower temperatures}$$



Heterojunction Bipolar Transistor - HBT

Differing semiconductor materials \Rightarrow Heterojunction

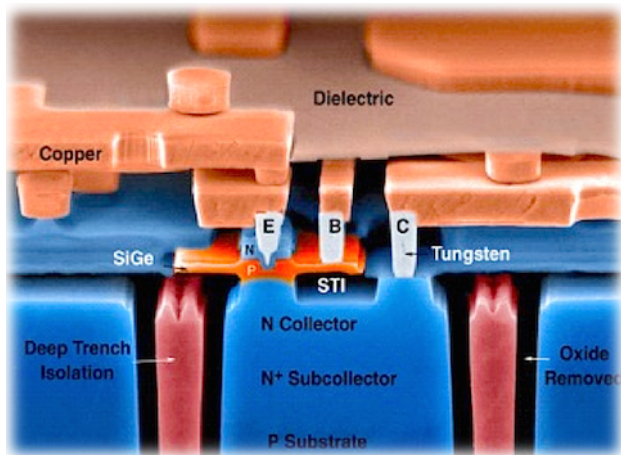
of one, at least, of the junctions of a bipolar transistor

\rightarrow **high frequency performances**

- **III-V or IV-IV hetero-junctions** are used by using InP/InGaAs or **Si/SiGe** for instance.
- Si/SiGe is one of the few hetero-junction **compatible with standard Si based technology**
SiGe HBT becomes the most popular bipolar technology with competitive speed, and even better, than III-V expensive technologies



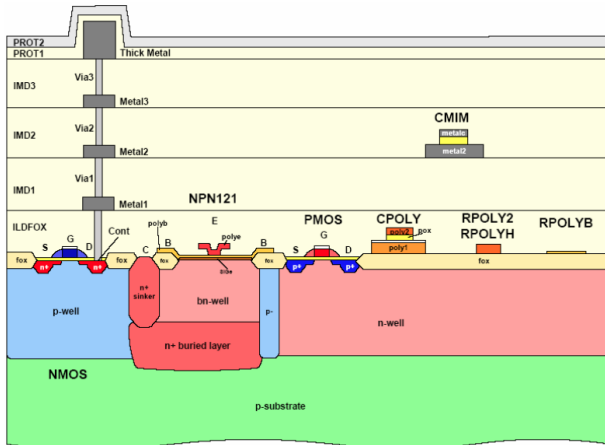
HBT planar technology



SiGe HBT - J.D. Cressler - Georgia Tech.



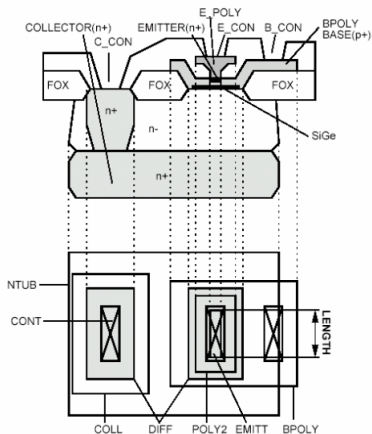
HBT planar technology



AMS BiCMOS SiGe 0.35µm



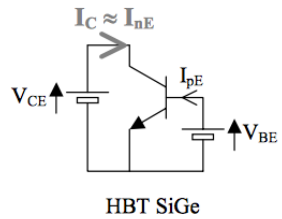
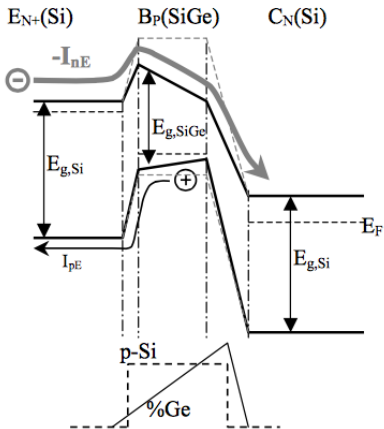
HBT planar technology



AMS BiCMOS SiGe 0.35 μ m



HBT planar technology



Instru. Cryo. SiGe - PhD D. Prêle



SiGe and cryogeny

- HBT is usually developed to achieve **high frequencies** perf.
- For **Cryogenic** applications, alloy of silicon and germanium (SiGe)

⇒ Change the $\beta(T)$

⇒ Pushes the **freeze-out** at lower temperatures

Si/SiGe heterojunction improve the **emitter injection efficiency**, as compare to BJT, so that it is possible to **increase the base doping**

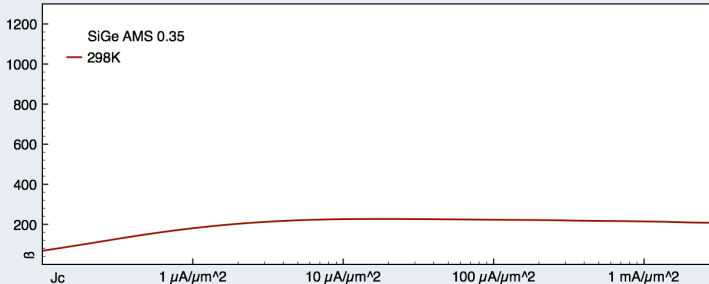
⇒ **SiGe HBT still work at 4.2 K**, far away temperatures where Si BJT is freezeed out



HBT current gain could increase exponentially with decreasing temperature

$$\beta_{SiGe} \propto \exp \frac{\Delta E_g}{k_B T} \quad \text{with} \quad \Delta E_g = \underbrace{E_{gE} - E_{gB}}_{<0 \text{ for BJT due to doping}} \approx \underbrace{E_{gE_{Si}} - E_{gB_{SiGe}}}_{\text{could be } >0 \text{ due to Ge}}$$

$\beta(T)$ and "band gap vs doping"



- at small J_C : recombinations in the base
- at large J_C : high injection

$$\beta(J_C) \xrightarrow{T \searrow} \text{"bell curve"}$$

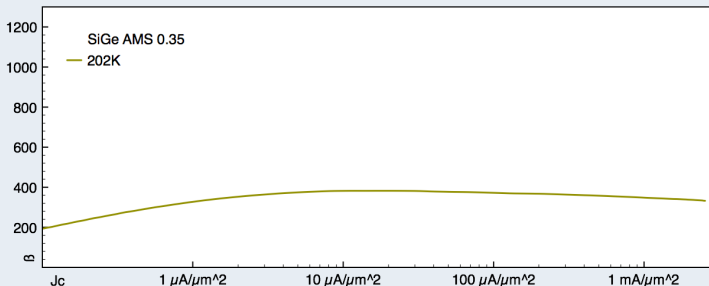
Transistor geometry \rightarrow current density (match the area for a I_C)



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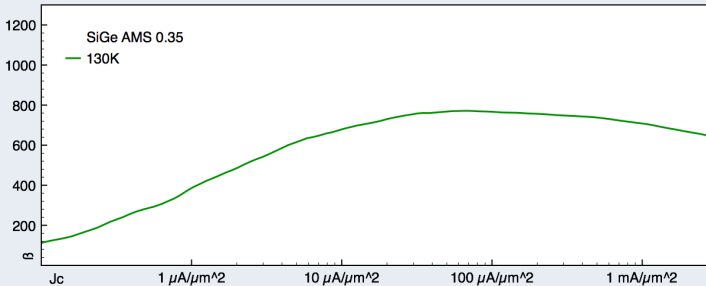
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$$\beta(J_C) \xrightarrow{T \downarrow} \text{"bell curve"}$$

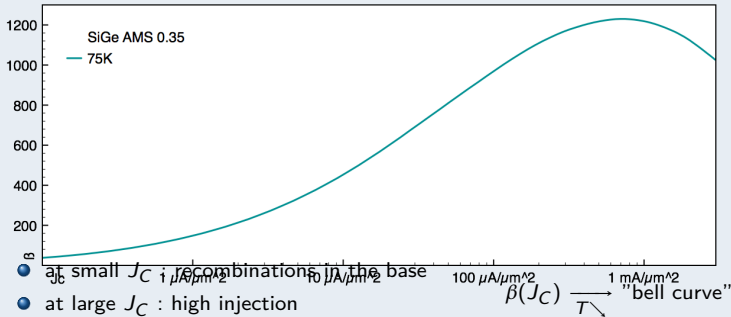
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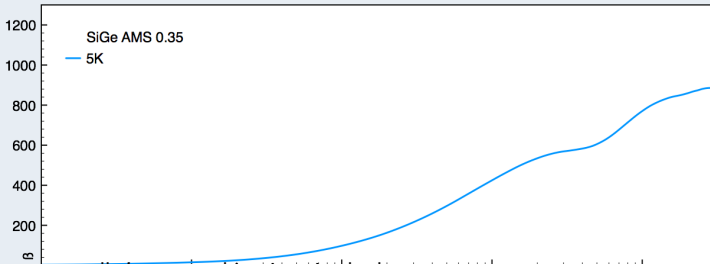
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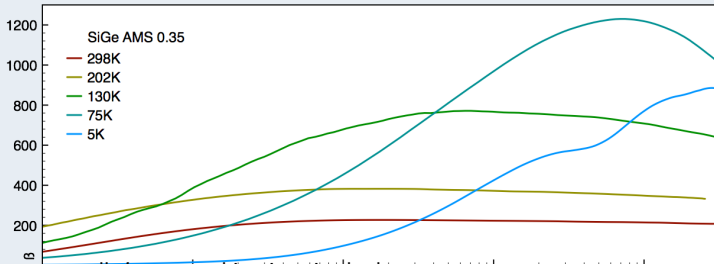
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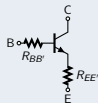


HBT transconductance

As for, BJT, the SiGe HBT transconductance follows

$$g_m = \frac{\frac{qI_C}{\eta k_B T_e}}{1 + R' \frac{qI_C}{\eta k_B T_e}}$$

$$\text{with } R' = \frac{R_{BB'}}{\beta} + \frac{(\beta+1)R_{EE'}}{\beta}$$

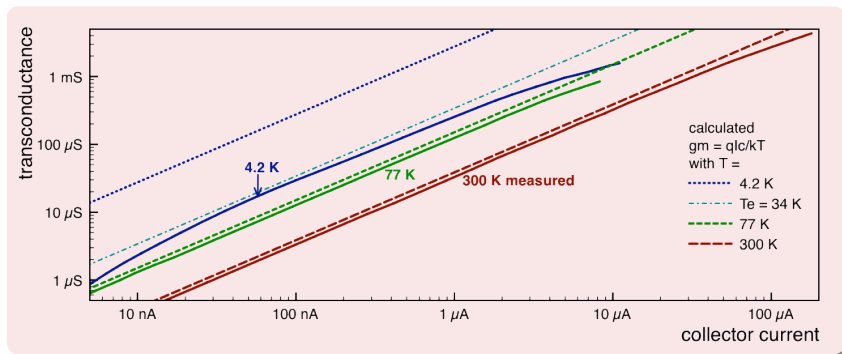


Below 77 K, the HBT still operates ...

- **Strong T_e decoupling**
- "Start" of freeze-out $\Rightarrow R' \nearrow$
- R' effect if $R' \frac{qI_C}{\eta k_B T_e}$ is comparable or larger than 1
 - Large R'
 - Large I_C
 - Low T



measured SiGe transconductance

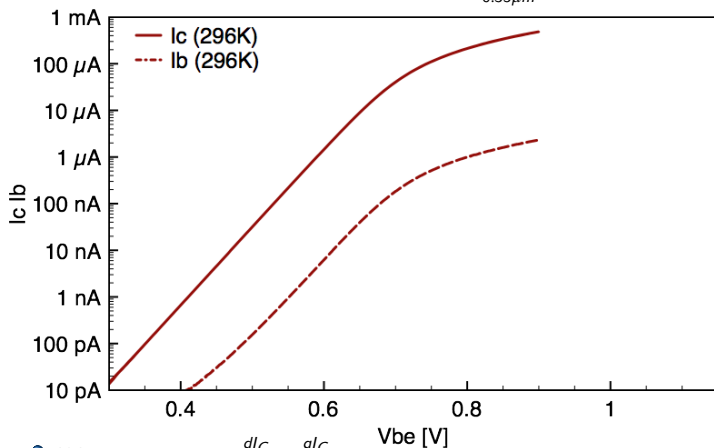


non-idealities

- $T_e \rightarrow$ the 4.2 K measurement fit with $qI_C/k_B 34$ K
- R' reduce the measured g_m (as compare to the ideal law)
- Recombination in the base-emitter depletion region at cryo. T



HBT parameters determined from pummel plots

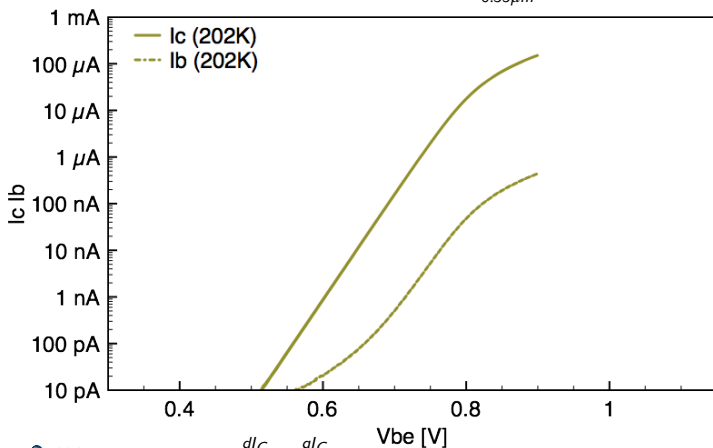
Gummel plot of a NPN254 SiGe_{AMS}0.35 μm ($L_E = 50\mu\text{m} \rightarrow \text{area} = 20\mu\text{m}^2$)

- Voltage gain $\Rightarrow g_m = \frac{dI_C}{dV_{be}} \approx \frac{qI_C}{k_B T}$

- Input impedance $\Rightarrow h_{11} = \frac{\beta}{g_m}$ and $\beta = \frac{I_C}{I_B}$; Buffer output impedance $\Rightarrow \frac{1}{g_m}$



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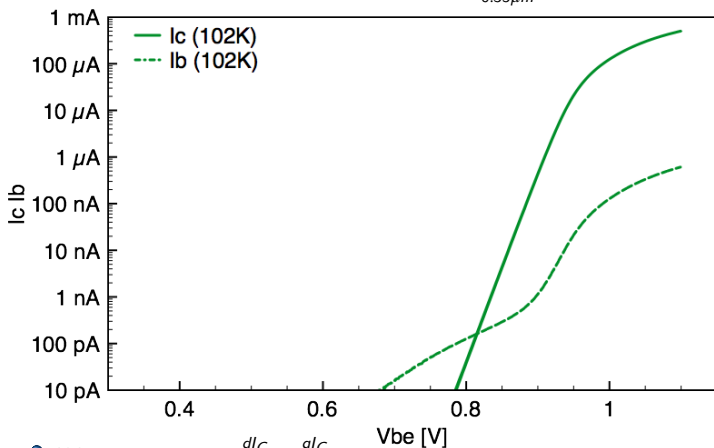
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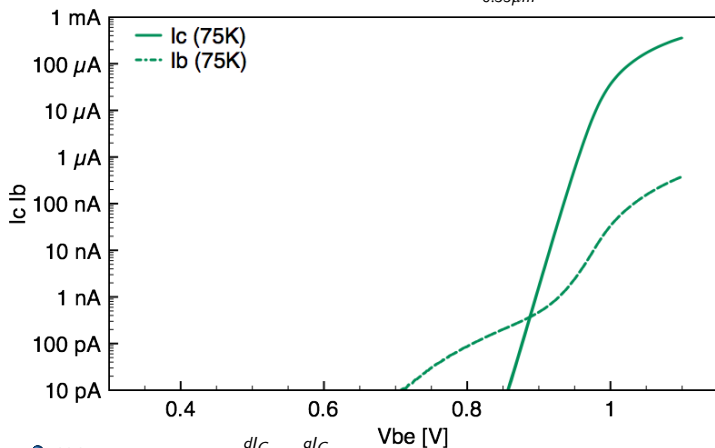
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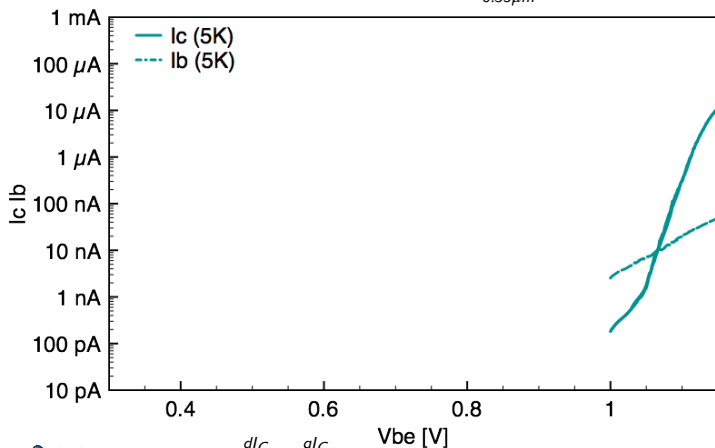
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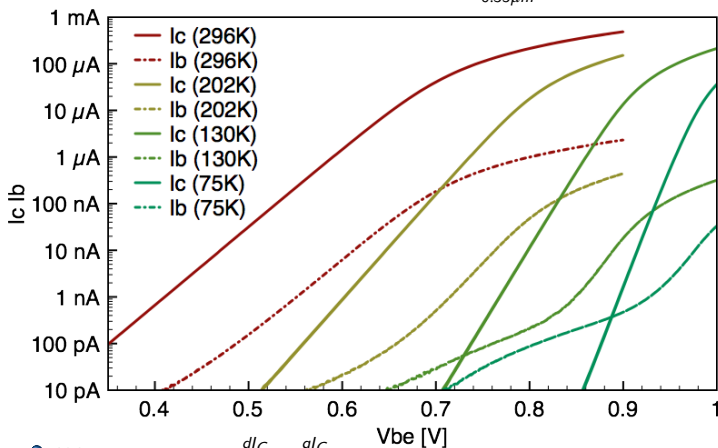
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Calculated h_{11} from β and g_m measurements

input impedance h_{11}

$$h_{11} = \frac{\beta}{g_m}$$

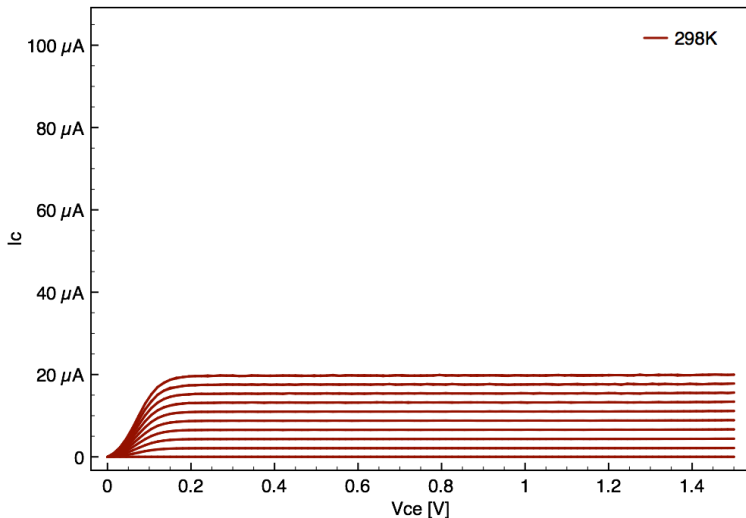
Considering a HBT SiGe with $100 \mu\text{m}^2$ area and $I_C = 1 \text{ mA}$

- J_C is thus equal to $10 \mu\text{A}/\mu\text{m}^2$ ($1 \text{ mA}/100 \mu\text{m}^2$)

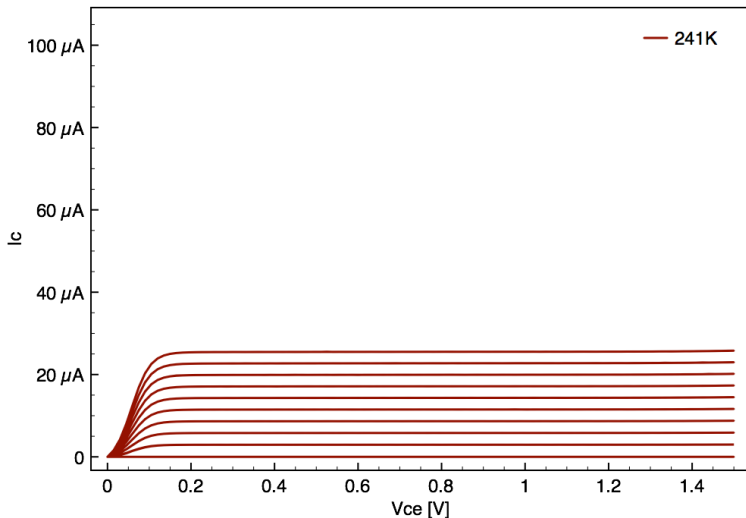
Parameters	300 K	77 K	4.2 K
β	180	1400	900
g_m	30 mS	100 mS	150 mS
h_{11}	6 k Ω	14 k Ω	6 k Ω



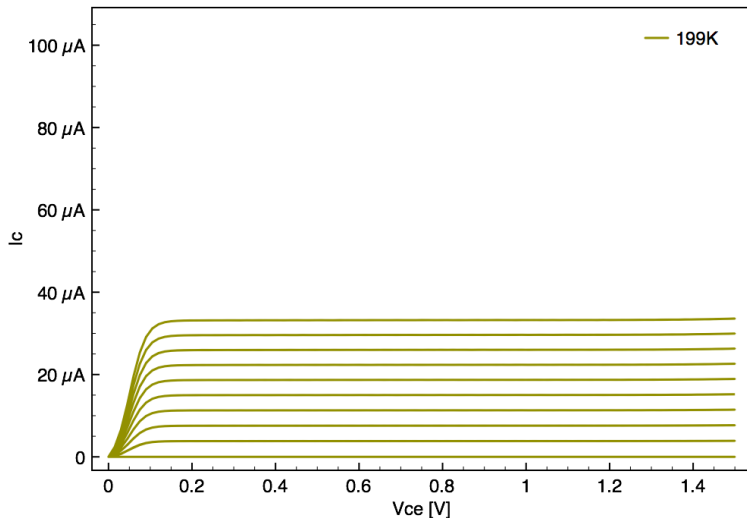
HBT $I_c(V_{ce})$ characteristic $\rightarrow V_{ce}$ offset



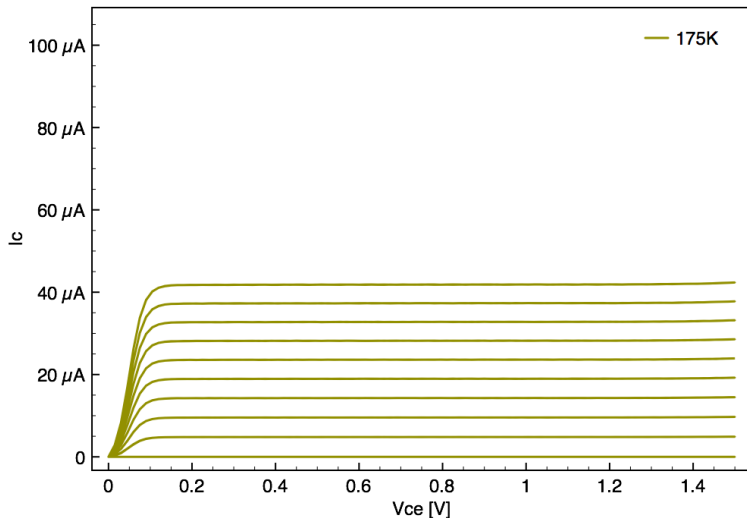
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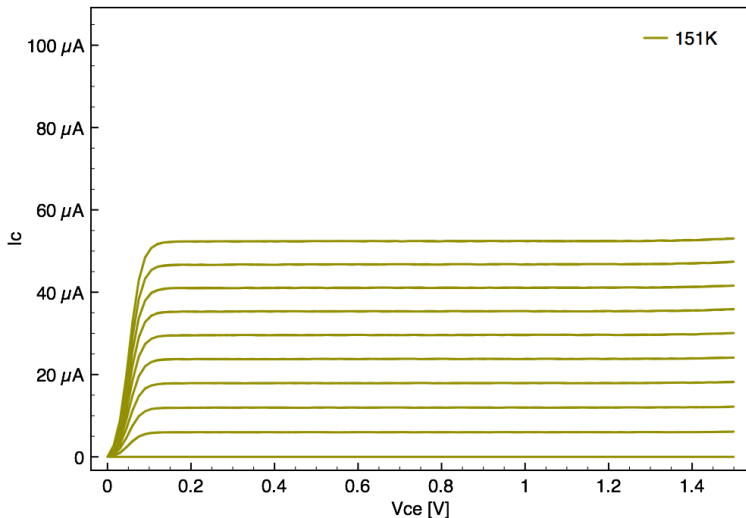
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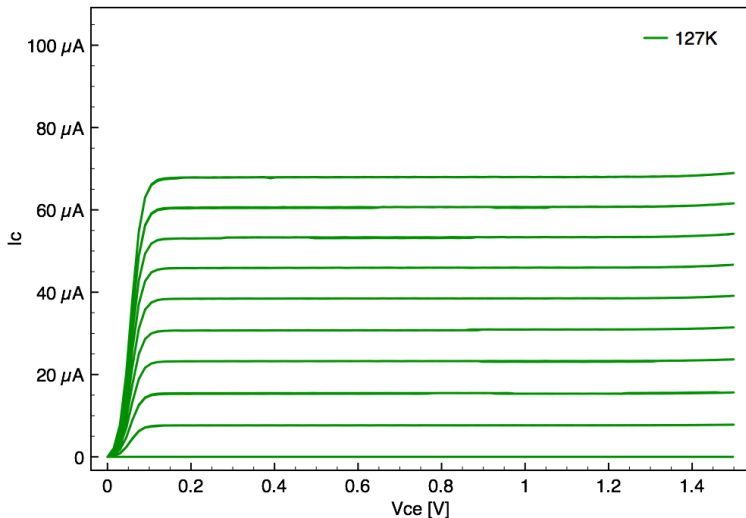
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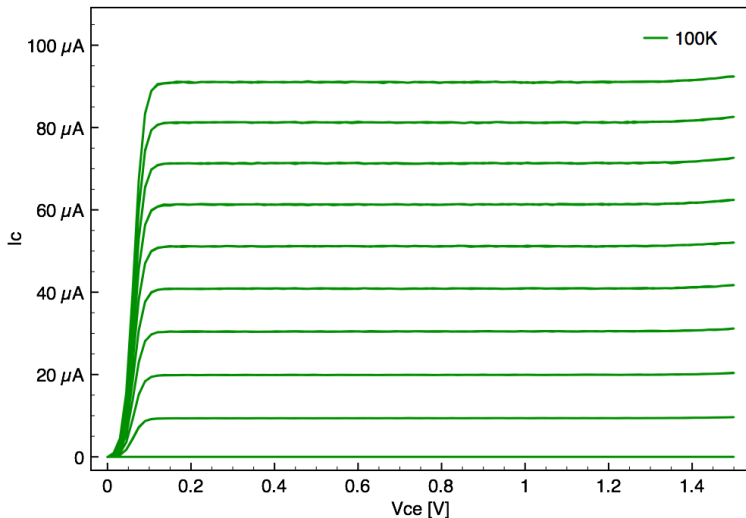
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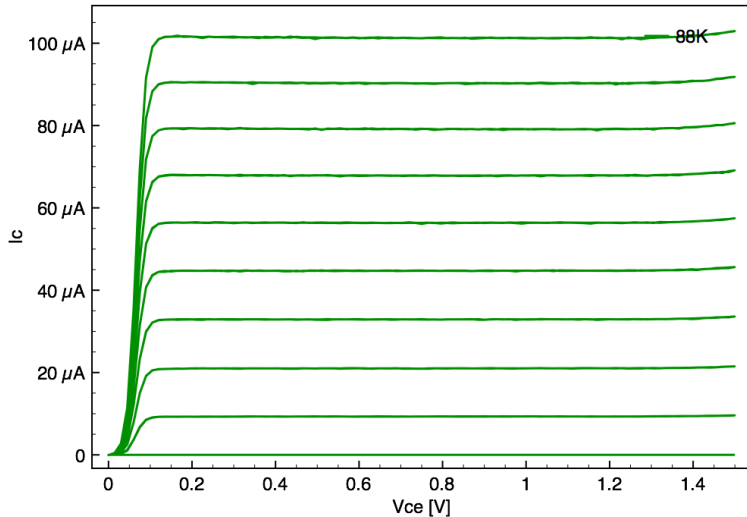
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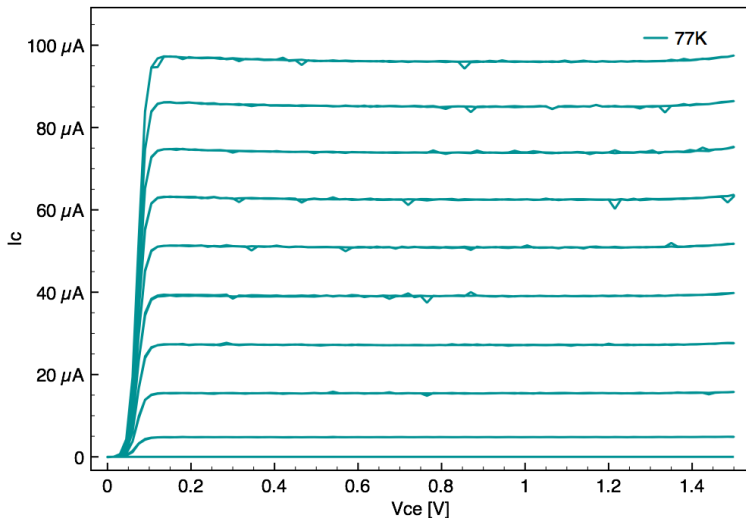
HBT $I_c(V_{ce})$ characteristic $\rightarrow V_{ce}$ offset



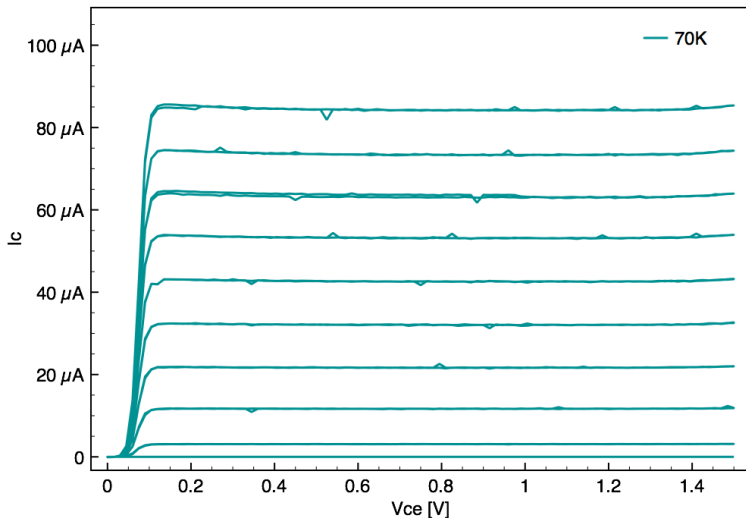
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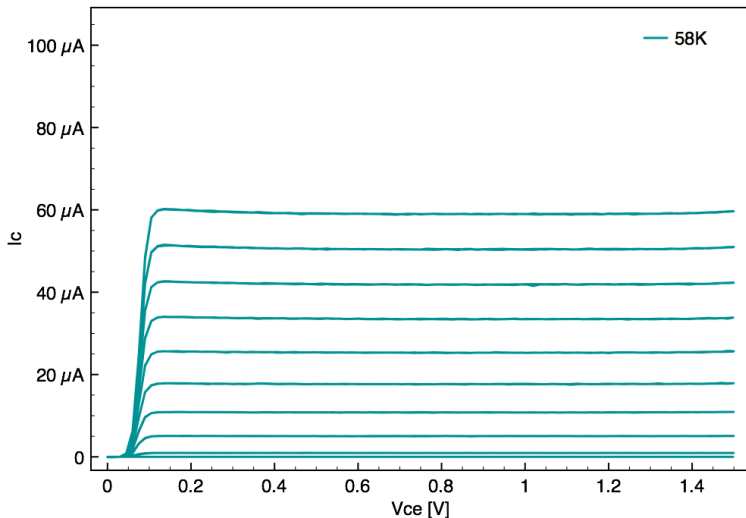
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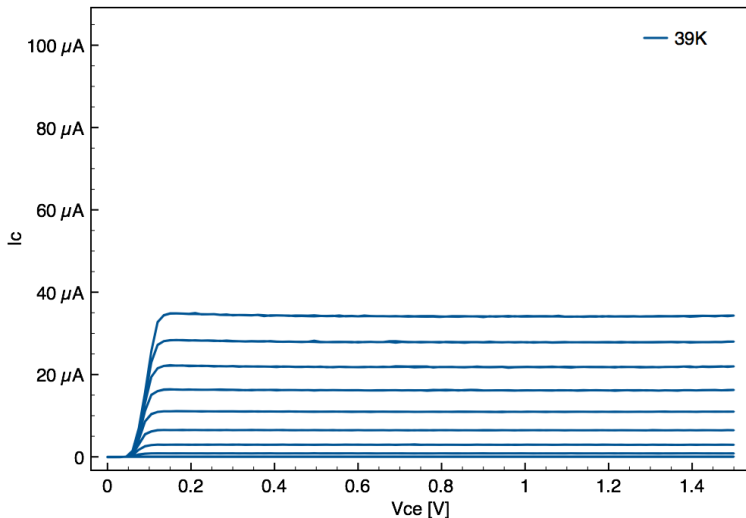
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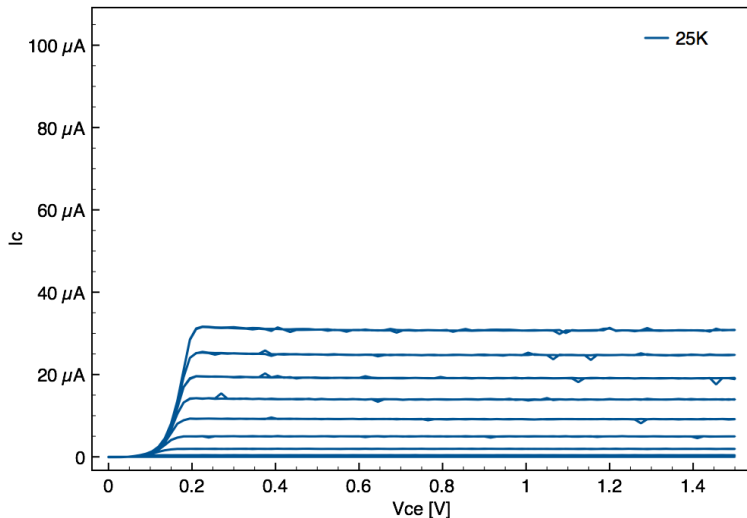
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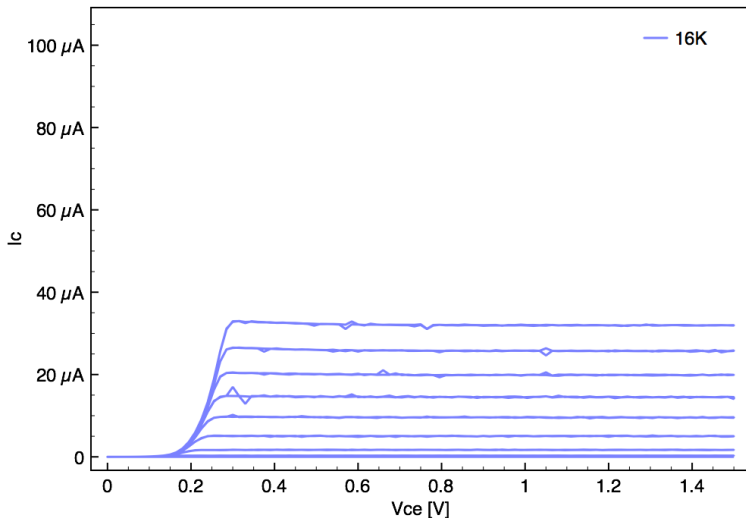
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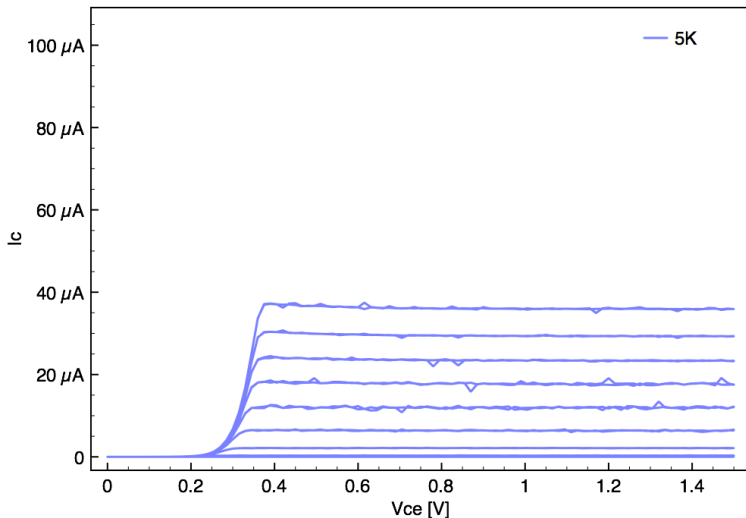


HBT $I_c(V_{ce})$ characteristic $\rightarrow V_{ce}$ offset



HBT $I_c(V_{ce})$ characteristic $\rightarrow V_{ce}$ offset



HBT $I_c(V_{ce})$ characteristic $\rightarrow V_{ce}$ offset

Noise discussion - on the benefit to have the larger g_m

FET noise = THERMAL noise of the channel resistance

- Output current noise : $S_{i_D} = 4k_B T \frac{2g_m}{3} + K \frac{I_D^{\alpha \approx 2}}{f^{\gamma \approx 1}}$
- **Input voltage noise** : $S_{V_{GS}} = \frac{S_{i_D}}{g_m^2} = \frac{8k_B T}{3g_m} + \frac{K}{g_m^2} \frac{I_D^{\alpha \approx 2}}{f^{\gamma \approx 1}}$

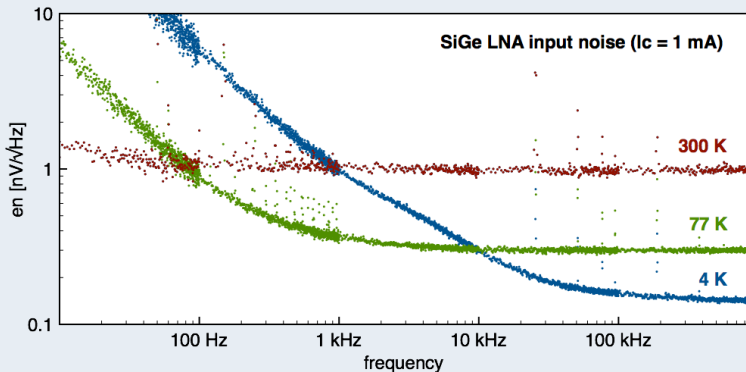
Bipolar noise = SHOT noise of the junctions

- **Input voltage noise** $S_{V_{BE}} = 4k_B T R_{BB'} + \frac{2qI_C}{g_m} + K \frac{R_{BB'} I_B^{\alpha \approx 2}}{f^{\gamma \approx 1}}$
 $\approx \frac{4k_B T}{2g_m} + K \frac{R_{BB'} I_B^{\alpha \approx 2}}{f^{\gamma \approx 1}}$
- Input current noise $S_{i_B} = 2qI_B + K \frac{I_B^{\alpha \approx 2}}{f^{\gamma \approx 1}}$



SiGe HBT Shot noise and 1/f (?) noise at cryo. T

1/f noise or sensitivity to the thermal fluctuations?

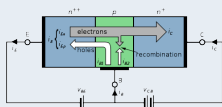


$$e_n \approx \frac{\sqrt{2qI_c}}{g_m}$$

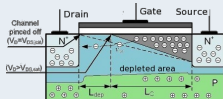
with $g_m \approx \frac{qI_c}{k_B T} \Rightarrow I_c$ fixed by the required input noise



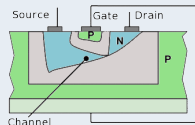
1/f noise and transistor topology



1/f noise is essentially due to the **non-ideal base current** in bipolar technologies



for MOS its cause come from the **trap on the oxide/channel interface** at the surface of the substrate



JFET channel is geometrically limited only by depleted regions → Less trap than near the surface → **Low 1/f noise**

+ effect of the size → $1/f \propto 1/\text{Area}$



Outline

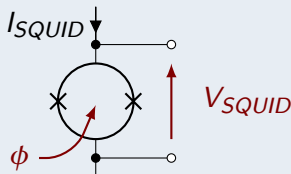
- 1 Analog multiplexers
 - Multiplexing as a modulation
 - Time domain multiplexing
 - Frequency domain multiplexing
- 2 Cryo-electronics
 - Cryogenic electronic devices
 - Semiconductor active devices
 - SQUID a superconducting active device
- 3 Applications
 - Millimeter domain to IR
 - Visible domain and scintillation
 - X domain



Superconducting QUantum Interference Device

SQUID = Magnetic flux transducer \Rightarrow Voltage

The "DC SQUID" is composed of one superconducting ring (Washer) interrupted by two Josephson junctions (x).



Very sensitive magnetometer which combine two physical phenomena :

- 1 **Magnetic flux quantization** ($\phi_0 = \frac{h}{2e} \approx 2.10^{-15} \text{ Wb}$ ou $[\text{T.m}^2]$ ou $[\text{V.s}]$) **in a superconducting loop**
- 2 **Josephson tunneling effect**



Magnetic flux quantization in a superconducting ring

Quantum properties of the superconductivity : $q = 2e$ (charge of the Cooper pair)

Superconductor is described by a **quantum wave function ψ** .

In superconducting ring, phase of ψ continuously change but **must comes to the same value around a turn** → magnetic flux screening can only compensates n magnetic flux quanta ϕ_0 :



$$\phi = n \frac{h}{2e} = n\phi_0$$

$\phi_0 = \frac{h}{2e} \approx 2.10^{-15} \text{ Wb}$ ou $[T.m^2]$ ou $[V.s]$ le quantum de flux magnétique

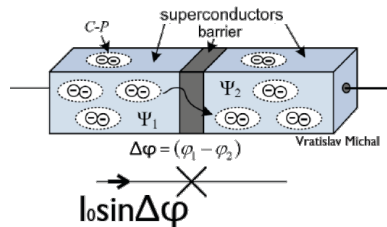


Josephson junction

2 superconductors separated by a thin ($\approx 10\text{nm}$) non-superconducting barrier.

Josephson tunneling effect :

Cooper pairs of electrons pass through the barrier by tunneling effect, maintaining phase coherence in the process.



Current biasing controls **phase difference $\Delta\phi$ between the two superconductor** according $I = I_0 \sin \Delta\phi$ leading to superconducting **phase modulation**.



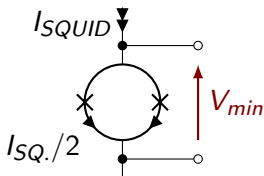
Interferences

For $I > I_0 \Rightarrow$ **voltage across the junction became >0**

Superconducting phase difference evolves evolves with time at the \rightarrow **Josephson frequency** :

$$I \approx I_0 \sin\left(2\pi \frac{V}{\phi_0} t\right) \Rightarrow \frac{f}{V} = \frac{1}{\phi_0} \approx 500 \text{MHz}/\mu\text{V}$$

SQUID provides at low frequency, average value of interferences.

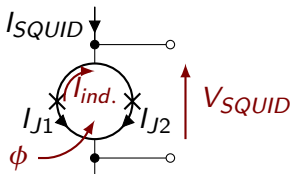


With no magnetic flux, the 2 junctions oscillate in phase
 \Rightarrow **destructive interference.**



Flux and superconducting phase shift

Magnetic flux leads to an additional phase shift $2\pi \frac{\phi}{\phi_0}$



$$I_{J1} \approx I_0 \sin \left(2\pi \frac{V}{\phi_0} t - 2\pi \frac{\phi}{\phi_0} \right)$$

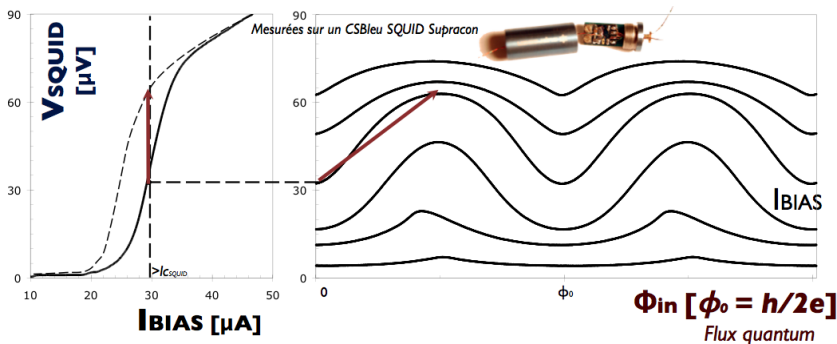
$$I_{J2} \approx I_0 \sin \left(2\pi \frac{V}{\phi_0} t + 2\pi \frac{\phi}{\phi_0} \right)$$

The two junctions are not in phase for $\phi \neq n\phi_0$ (periodicity)



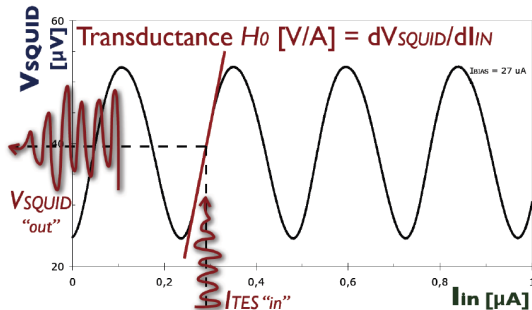
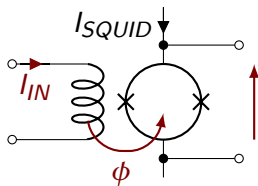
I(V) and V(ϕ) characteristic SQUID (Magnetometer)

- Bias $< 2I_0$: no voltage
- Bias $> 2I_0$: SQUID has periodic (ϕ_0) characteristic V(ϕ)



SQUID as a trans-impedance amplifier

An input loop is used to convert I_{IN} in flux $\phi = \frac{I_{IN}}{M_{IN}}$:



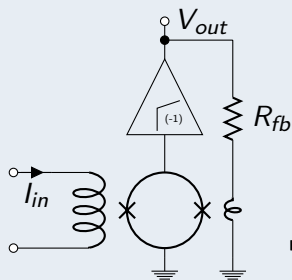
- Input impedance = 0Ω
- Input noise $\approx pA/\sqrt{Hz}$
- Trans-impedance gain $\approx 100 V/A$



A flux feedback to linearize the SQUID characteristic

An other loop is usually used to compensate magnetic flux induced by I_{in} .

Flux Locked Loop



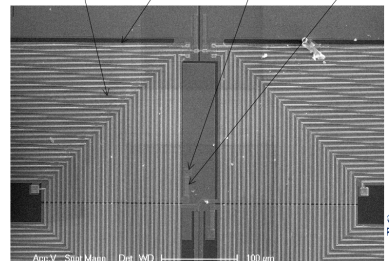
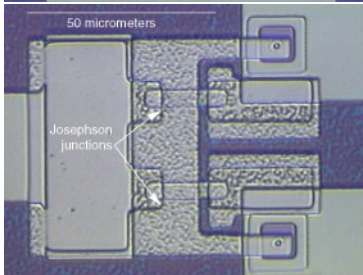
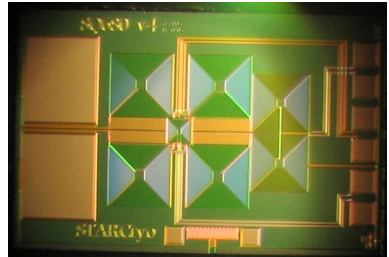
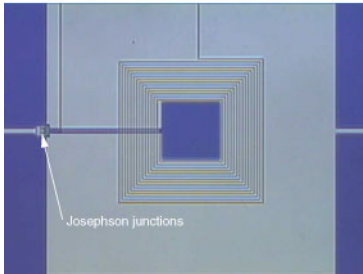
$$|H_{open}| = \left. \frac{V_{out}}{I_{in}} \right|_{open} = H_{0SQUID} G_{Amp}.$$

$$|H_{FLL}| = \left. \frac{V_{out}}{I_{in}} \right|_{close} = \boxed{\frac{M_{in}}{M_{fb}} R_{fb}}$$

☞ Don't worry about the loop gain sign, H_0 is periodic!



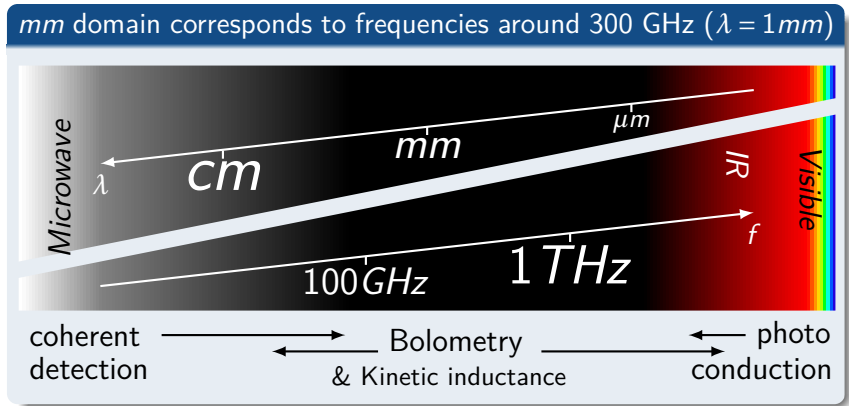
Planar technology and gradiometry



Outline

- 1 Analog multiplexers
 - Multiplexing as a modulation
 - Time domain multiplexing
 - Frequency domain multiplexing
- 2 Cryo-electronics
 - Cryogenic electronic devices
 - Semiconductor active devices
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 - X domain





Main interest of the *mm* domain in cosmology :

- Observation of the cosmic microwave background (CMB) thermal black body spectrum at a temperature of 2.7 K

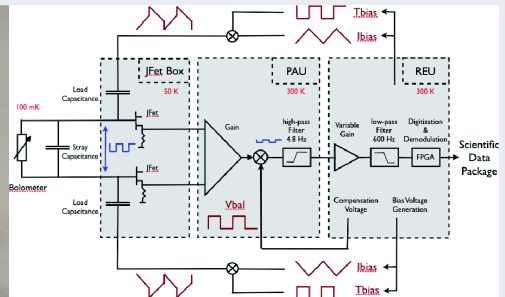
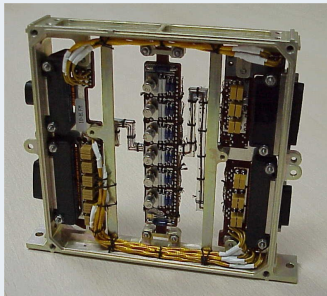
The instrument is usually cooled to 100-300 mK !!



The use of a cryogenic JFet stage for *mm* detection



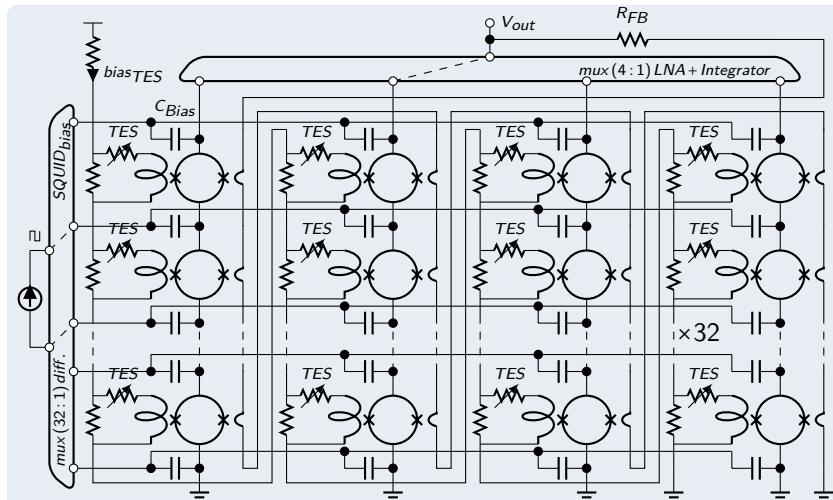
Planck-HFI JFet Box (Semicon. bolo. readout chaine) - NOT multiplexed



- JFET source followers to reduce the semicond. bolo impedance
- JFETs thermally insulated to keep the **optimal temperature of 110 K**
- 240 mW, mainly produced by the JFETs and the source resistors
- $3 \text{ nV}/\sqrt{\text{Hz}} \Rightarrow$ less than 5% of the total readout noise



Cryogenic TES time domain multiplexer - QUBIC

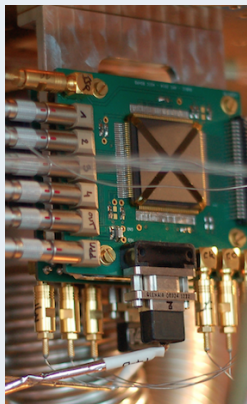
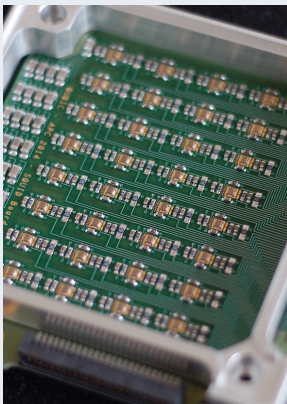
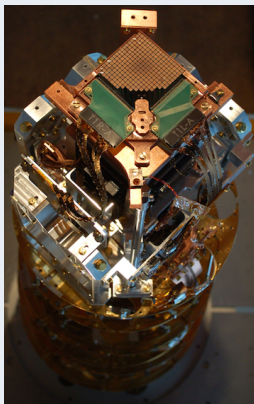


D. Prêle, F. Voisin et al, "Capacitively-coupled SQUID Bias for Time Division Multiplexing", Journal of Low Temperature Physics, 2014



Cryogenic TES time domain multiplexer - QUBIC

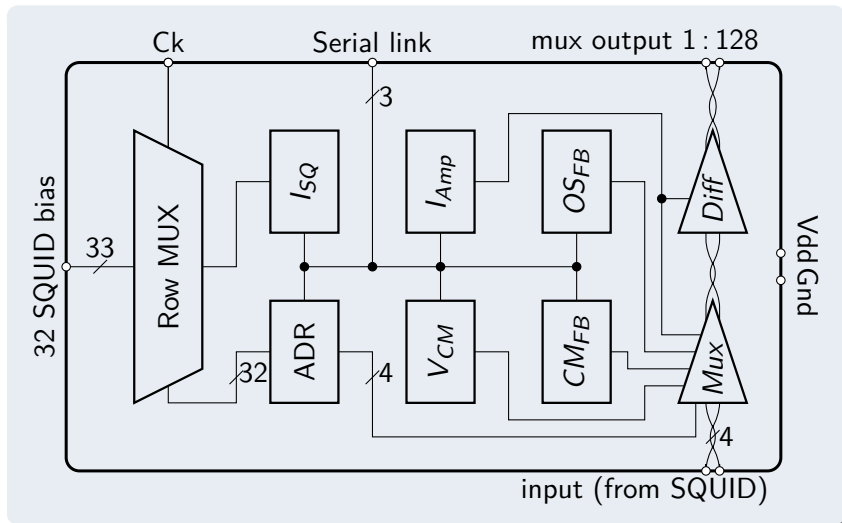
QUBIC readout chaine : TES (300 mK) + SQUID (1K) + ASIC (77K)



Correlated sampling on blind thermometers to remove $1/f$ noise



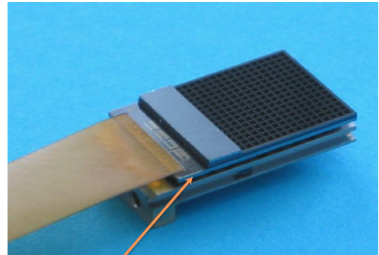
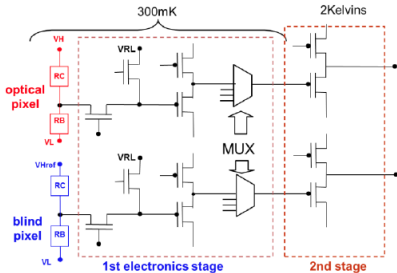
SiGe ASIC for cryogenic 1 :128 TDM



300 mK CMOS 1 :16 TDM - PACS/Herschel satellite



- **Double correlated sampling** to remove $1/f$ readout noise
- **Differential** measurement with blind pixels to remove the external collective perturbations.



cold electronics layer





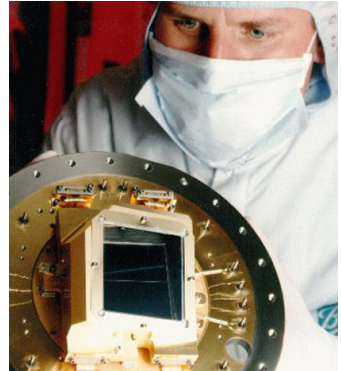
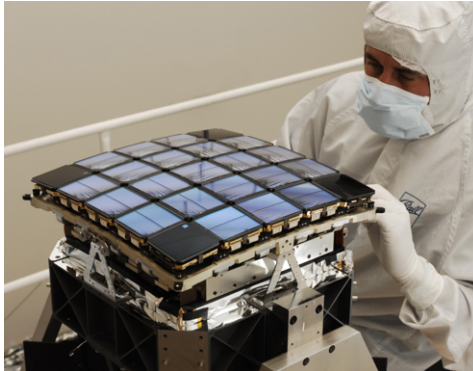
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CCD (Charge Coupled Device) in astronomy

CCD is widely used in astronomy (examples : Kepler  and Hubble )
to achieved **high-quality image** despite a low photon flux
- high quantum efficiencies.



NASA/ESA and Ball Aerospace

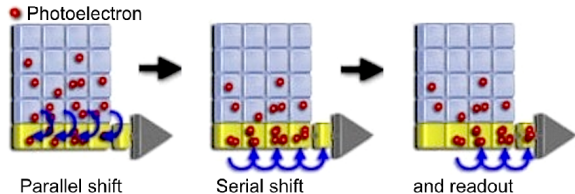


CCD - Charge-Coupled Device : Charge Transfert \equiv TDM

- **CCD** was **invented in 1969** by Boyle & Smith - Bell Labs
- They were **Physics Nobel Prize 2009**, for the CCD concept

CCD technologies are based on array of sensors using **photoelectric effect**. However, **discovery of the law of the photoelectric effect** (photon to e^- conv.) is the "**Einstein Nobel Prize 1921**"

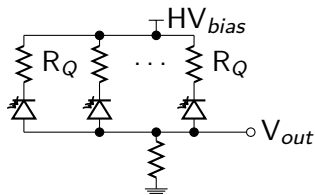
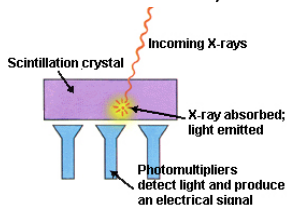
\Rightarrow Reconised as new in the CCD, is the readout technic based on the **charge transfer** : *Parallel-in Serial-out shift register*



Photon sensitive detectors for "calorimetry"

Ultra sensitive detection and high energy astrophysics indirect detection

Solid state photomultiplier (SiPM) used for high energy calorimetry (measure of the energy of the high energy photon). SiPM are the **summation, with no modulation** of photon sensitive sensors.



SiPM cryogenic operation down to 77 K - D. Prele et al

Cooling required to decrease the noise (DCR)

Some time due to natures of scintillators (Liquid xenon or argon for dark matter direct detection)



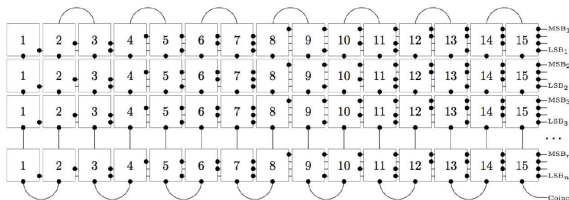
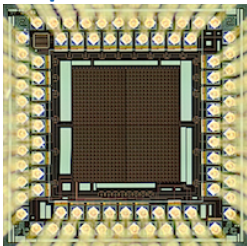
Photon sensitive imager

Gamma astro need to have the direction of the gamma sources.

A way to do that is proposed by the "gamma cube" concept

The Gamma Cube : a novel concept of gamma-ray telescope - F. Lebrun et al..

A photon sensitive imager = a coding in the SiPM concept :



Sub array coding allows to determine what is the hit pixel. Operate with a very low photons flux

The Gamma Cube : a new way to explore the gamma ray sky - F.

Lebrun, R. Terrier, D. Prêle, D. Pellion et al



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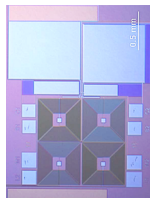
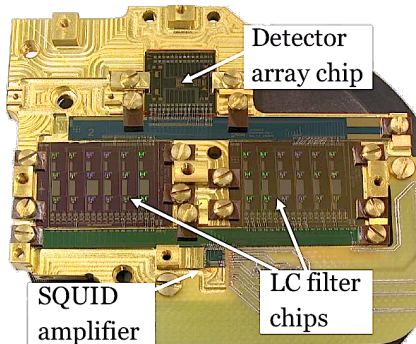


TES Frequency Domain Multiplexing

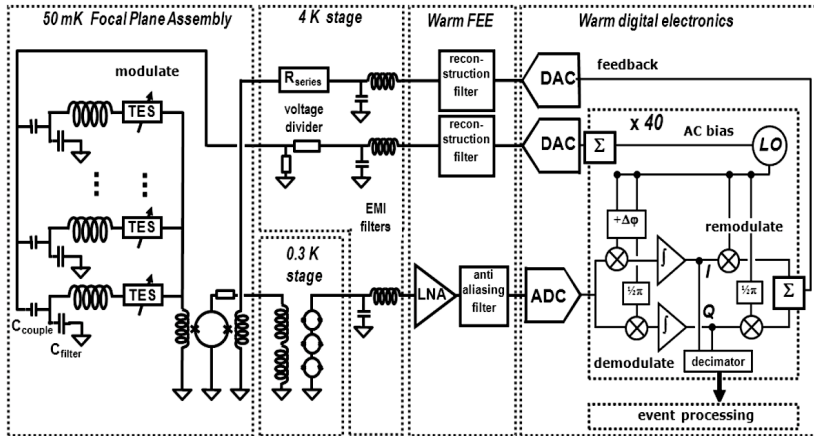
- Array of TESs (**Transition Edge Sensors**) are used in astronomy (mm and X-ray)
- Athena is a proposed ESA X-ray observatory



One of the instrument is based on **TES array + FDM** :



TES Frequency Domain Multiplexing - LC resonators

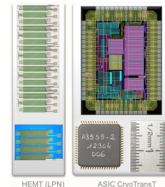
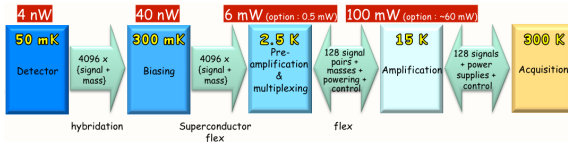
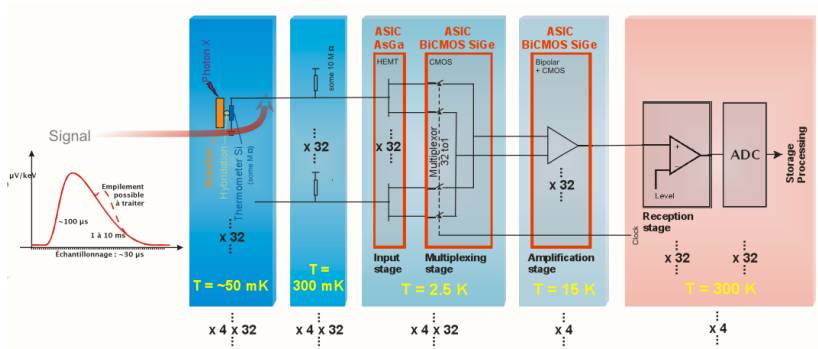


Athena XIFU BBFB - Hartog et

A1



X-ray microcalorimeter + TDM (HEMT + SiGe)



X. de le Broÿse et al. - CEA SEDI



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- Semiconductor devices for cryogenic amplification (WOLTE10 - D. Prêle)

